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A slab type gas laser is known as one type of gas lasers such as CO<sub>2</sub> (carbon dioxide) laser. In a slab type gas laser, the gap between excitation electrodes is narrow so that the excited gas colliding with the electrodes is cooled, thereby accelerating the release of laser lower level. This is the reason why the laser is known as an electrode diffusion cooling type laser.

A known cylindrical straight slab type gas laser comprises a pair of cylindrical electrodes of different diameter disposed horizontally and concentrically by way of spacers. The gap between the two cylindrical electrodes is filled with laser medium to define a cylindrical straight slab. A ring-shaped trick mirror is disposed at one end of the cylindrical straight slab and an output mirror (half mirror) is disposed at the center of the one end to pass a part of the light and to reflect a part of the remaining light. A w-axicon mirror is disposed at the other end of the cylindrical straight slab.

## Summary of the Invention

Unfortunately, however, the use of such spacers causes split, non-uniform peaks and split, non-uniform beam in a far-field image focused by a lens. Any laser beam other than Gaussian distribution profile is impractical for a cutting machine because cutting width and cutting efficiency vary depending on the direction of movement of the beam.

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## Brief Description of Drawings

Now, the present invention will be described in greater detail by reference to the accompanying drawings, wherein :

FIG. 1 is a cross section view (A) and a side view (B) of one example of a conventional cylindrical straight slab type gas laser :

FIG. 2 shows a laser beam intensity distribution at the exit of an output mirror of the gas laser as shown in FIG. 1 :

FIG. 3 shows an intensity distribution of a far-field image of the laser beam as shown in FIG. 2 focused by a lens :

FIG. 4 is a simplified view of a preferred embodiment of the cylindrical straight slab type gas laser according to the present invention :

FIG. 5 shows 3 kinds of trick mirrors having different center offsets to be used in the slab type gas laser :

FIG. 6 shows a laser beam intensity distribution at the exit of the output mirror of the gas laser as shown in FIG. 4 : and

FIG. 7 is intensity distributions of far-field images of the beam as shown in FIG. 6 focused by a lens.

## Description of the Preferred Embodiments

For better understanding of an embodiment of the present invention, a conventional cylindrical straight slab type gas laser will be described first by reference to FIG s . 1—3. FIG. 1 (A) is a cross section view and FIG. 1 (B) is a side view of a conventional cylindrical straight slab type gas laser. As illustrated in FIG. 1, the cylindrical straight slab type gas laser comprises a pair of concentrically and horizontally disposed cylindrical electrodes 11, 12 of different diameter by way of spacers 13. The gap between the two cylindrical electrodes 11, 12 is filled with laser medium to define a cylindrical straight slab 1. A ring-shaped trick mirror M1 is disposed at one end of the cylindrical straight slab 1. Also disposed at the center of the one end of the cylindrical straight slab 1 is an output mirror (half mirror) M2 to pass a part of the light and to reflect a part of the remaining light. A w-axicon mirror M3 is disposed at the other end of the cylindrical straight slab 1.

As mentioned above, the cylindrical straight slab type gas laser employing the cylindrical straight slab 1 uses the trick mirror M1 as shown in FIG. 5 (C) in order to increase the output. That is, the center offset  $X_m$  (the distance of the center of curvature from the center axis) of the trick mirror M1 is set larger than the center position  $X_0$  (the distance between the midpoint of the width from the center axis) of the trick mirror itself.

Such slab type gas laser cannot provide an excellent mode beam having substantially Gaussian intensity distribution at the focused profile as shown in FIG. 7 (A) and (B) and may exhibit non-uniform split beam intensity distributions as shown in FIG. 3 (A) and (B) unless operated with accurate concentric positioning of the two cylindrical electrodes 11, 12. This is the reason why a plurality of spacers 13

are provided between the two cylindrical electrodes 11, 12 as illustrated in side view in FIG. 1 (B). However, such spacers 13 cause beam intensity distribution having split peaks and irregular peaks as shown in FIG. 2 at the exit of the output mirror M2. Also, far-field images of the laser beam in this mode focused by a lens are split and non-uniform as illustrated in FIG. 3 (A) and (B).

When the laser beam is used in a cutting machine, any laser beam departing from the Gaussian intensity distribution is impractical because cutting width and efficiency vary depending on the direction of movement of the laser beam.

The above mentioned problem associated with the conventional slab type employing cylindrical straight slab is solved by the cylindrical straight slab type gas laser according to the present invention that comprises two cylindrical electrodes of different diameter disposed concentrically by way of spacers. The gap between the two cylindrical electrodes is filled with laser medium to define a straight slab. A ring-shaped trick mirror is disposed at one end of the straight slab. An output mirror is disposed at the center of the one end of the straight slab to pass a part of the light therethrough while reflecting a part of the remaining light. A w-axicon mirror is disposed at the other end of the straight slab. It features to set the relationship between the center offset  $X_m$  of the trick mirror and the center position  $X_0$  of the trick mirror itself to  $X_m \leq 1.1 X_0$ .

(Preferred Embodiment)

Now, a preferred embodiment of the present invention will be described hereunder by reference to FIGs. 4—7. Illustrated in FIG. 4 is a simplified construction of the cylindrical straight slab type gas laser according to the present invention. A cylindrical straight slab 1 is defined by a pair of cylindrical electrodes 11, 12 of different diameter laying horizontally and concentrically by way of insulating spacers 13 and filling laser medium in the area defined by the pair of cylindrical electrodes 11, 12. A ring-shaped trick mirror M1 is disposed at one end of the cylindrical straight slab 1 and an output mirror (half mirror) M2 is disposed at the center of the one end of the cylindrical straight slab 1 for passing a part of the light and for reflecting a part of the remaining light. On the other hand, a w-axicon mirror M3 is disposed at the other end of the cylindrical straight slab 1.

When high frequency excitation voltage is applied between the two cylindrical electrodes 11, 12, the gas filled in the cylindrical straight slab 1 is excited and a laser beam is generated by a resonator comprising the three mirrors M1, M2 and M3 to be extracted from the output mirror M3.

Three kinds of ring-shaped mirrors are prepared as the trick mirror M1. As illustrated in FIG. 5 (A) ~ (C), they are different in radius of curvature and the center position of the curvature. Experiments are made to verify the relationship between the center offset  $X_m$  and the beam quality (closeness to the Gaussian distribution in the beam intensity profile)  $Q$  for each mirror. Experiment results prove that the emitted beam is the best when the following relationship between the center offset  $X_m$  and the center position  $X_0$  of the trick mirror M1 is satisfied  $X_m \leq 1.1 X_0$ .

1 That is, the beam at the exit of the output mirror M2 is split due to the use of the spacers 13 but exhibits  
2 uniform peaks as shown in FIG. 6. Far-field images of the laser beam in this mode focused by a lens are  
3 substantially Gaussian intensity distribution as shown in FIG. 7 (A) and (B) .

4 If the relationship between the center offset  $X_m$  and the center position  $X_0$  of the trick mirror M1 is set  
5 as specified above, there is a slight decrease in the total laser beam output. However, the far-field  
6 image of the laser beam focused by a lens provides substantially Gaussian intensity distribution that is  
7 useful in terms of cutting width and cutting efficiency when applied to a cutting machine.

8 As apparent from the above description of the preferred embodiment according to the present invention,  
9 the relationship between the center offset  $X_m$  and the center position  $X_0$  of the trick mirror M1 is set to  
10  $X_m \leq 1.1 X_0$  to provide a uniform beam having substantially Gaussian intensity distribution in the far-  
11 field image of the output laser beam focused by a lens even if the spacers 13 are employed. As a result,  
12 the output laser beam is suitable to be applied to a cutting machine.

13 Although the preferred embodiment of the cylindrical straight slab type gas laser according to the  
14 present invention is described herein, it is to be understood that the invention is not limited only to such  
15 embodiment and that various modifications can be made by a person having an ordinary skill in the art  
16 without departing from the scope and spirit of the present invention.